Material Unistrength (Universal Material Strength Science) Ph. D. & Dr. Sc. Lev G. Gelimson (AICFS)

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Material strength science uses nonuniversal dimensional mechanical stresses without expressing their risk (danger) degrees. For an arbitrarily anisotropic material with different resistances to tensions and compressions and for any variable loads with possibly rotating the principal directions of the stress state at a material point during loading, there are no common limiting state criteria for triaxial mechanical stresses and no universal strength laws of nature. The Tresca and Huber-von-Mises-Hencky criteria are quite nonsensitive to pressure with significant effect on strength in the Nobel prize winner Bridgman experiments and prescribe to the ratio of the tensile and shear strengths the values of 2 and 3^{1/2} whereas this ratio varies from 1 to 4.

Material unistrength [1-9] discovers universal stresses, or unistresses, σ_j° . For any stationary loading an arbitrarily anisotropic material, $\sigma_j^{\circ} = \sigma_j/|\sigma_{Lj}|$ where σ_{Lj} is, for the usual principal stress, σ_j , its limiting value which has the direction and sign of σ_j and acts at the same material's point, the both other principal stresses vanishing, and the other loading conditions at the same point being the same. Linearly correcting an arbitrary limiting criterion $\sigma_e = F(\sigma_1, \sigma_2, \sigma_3) = \sigma_L$ via constant x and generalizing give $\sigma_e = F(\sigma_1, \sigma_2, \sigma_3) + x\sigma_2 = \sigma_L, \sigma_e^{\circ} = F(\sigma_1^{\circ}, \sigma_2^{\circ}, \sigma_3^{\circ}) = 1, \sigma_e^{\circ} = F(\sigma_1^{\circ}, \sigma_2^{\circ}, \sigma_3^{\circ}) + x\sigma_2^{\circ} = 1$. See the limiting surfaces and lines in unordered principal stresses σ_{1u} , σ_{2u} , σ_{3u} in Figures 1, 2 for an isotropic material with equal strength in tension and compression (Figure 2 above) and with unequal strengths in tensions and compressions in the cases of isotropy (Figure 1, Figure 2 in the middle) and anisotropy (Figure 2 below):





Figure 1. $\sigma_e^{\circ} = F(\sigma_1^{\circ}, \sigma_2^{\circ}, \sigma_3^{\circ}) = 1$

Figure 2. $\sigma_e^{\circ} = F(\sigma_1^{\circ}, \sigma_2^{\circ}, \sigma_3^{\circ}) + x\sigma_2^{\circ} = 1$

For variably loading with initial mean cycle stress $\sigma_{m0j}(t)$ at time t in T = [t₀, t₁], $\sigma_j^{\circ}(t) = [\sigma_j(t) - \sigma_{m0j}(t)]/|\sigma_{Lj}(t) - \sigma_{m0j}(t)|$. For each uniaxial stress process, $\sigma_j(t)$, its own reserve, n_j , is defined by the similar limiting process, $n_j\sigma_j(t)$, with possibly taking damage accumulation into account. Determine the equidangerous cycle of unistresses with mean stress σ_{mj}° and amplitude stress σ_{aj}° , then the constantly vectorial reduced

unistress $\sigma_{j}^{\circ} = (\sigma_{mj}^{\circ}, \sigma_{aj}^{\circ})$ via the limiting amplitude diagram. Now choose the most dangerous, possibly depending on t, permutations of the stationary indexes, ju, of the unordered unistresses without $\sigma_{1u}^{\circ} \ge \sigma_{2u}^{\circ} \ge \sigma_{3u}^{\circ}$. The final universal criterion is

 $\sigma_{e^{\circ}} = \max\{\sup_{t \in T} \max_{ju(t)} F(\sigma_{1u^{\circ}}(t), \sigma_{2u^{\circ}}(t), \sigma_{3u^{\circ}}(t)), \max_{ju} |F(\sigma_{1u^{\circ}}, \sigma_{2u^{\circ}}, \sigma_{3u^{\circ}})|\} = 1.$ Material unistrength gives universal strength laws also for aeronautical fatigue.

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